



Sheet (4)

- (1) An inductive load of $R=10\ \Omega$ and $L=31.83\ \text{mH}$ is fed from 220-V 50-Hz ac supply via 1-phase controller uses phase angle control. For triggering angles of $\pi/4$, $\pi/2$, find:
- The extinction angle (β),
 - The conduction angle,
 - The max. and min. values of the voltage applied to the switch and
 - Draw typical waveforms for each part of the circuit.
- (2) A 1-phase ac phase angle controller feeds an inductive load of $R=10\ \Omega$ and $L=31.83\ \text{mH}$. The input supply voltage is 220-V, 50-Hz and the triggering angle is $\pi/3$. Find:
- The RMS value of the load voltage,
 - The RMS value of the fundamental component of the load voltage, and
 - The percentage of the fundamental component.
- (3) A 1-phase ac phase angle controller is fed from 220-V, 50-Hz ac supply and feeding an inductive load of $R=10\ \Omega$ and $L=55.13\ \text{mH}$. At triggering angle of $\pi/2$, find:
- The RMS values of the load voltage and current,
 - The power consumed by the load, and
 - The supply power factor.
- (4) At the instant of firing of a 1-phase ac phase angle controller, the forward voltage applied to the switch is 220V. The controller is fed from 220-V, 50-Hz ac supply and feeding an inductive load of $R=10\ \Omega$, if the output voltage is $0.96 V_s$. Find:
- The extinction angle (β),
 - The RMS load voltage, and
 - The load inductance (mH).
- (5) A single phase Transformer Tap Changer; its primary voltage is 208V, 60Hz and its secondary voltages are $V_{s1}=120\text{V}$ and $V_{s2}=88\text{V}$. If the load resistance is $5\ \Omega$ and the RMS load voltage is 180V, determine:
- The delay angles of thyristors T_1 and T_2 ,
 - The RMS current of all thyristors,
 - The input power factor, and
 - The maximum power that can be delivered to the load.
- (6) A TRIAC Light Dimming Circuit is to be designed for a 100W filament lamp working from a 220V, 50Hz source. The capacitor of $0.05\ \mu\text{F}$, an adjustable resistance R and a DIAC with breakover voltage of 40V are used. Determine the lowest RMS voltage down to which adjustment is possible if $R=3\text{K}\Omega$.



(1) Expressions of AC voltage controller

(I) On/off control

$$\text{duty cycle, } k = \frac{t_{on}}{t_{on} + t_{off}} = \frac{n}{n+m}$$

RMS value of the load voltage,

$$V_o = V_s \sqrt{k}$$

Active power,

$$P = \frac{V_s^2 \sqrt{k}}{R}$$

Supply power factor,

$$\text{Pf} = \sqrt{k}$$

(II) phase angle control

(i) RMS of load voltage

$$V_o = V_s \sqrt{\frac{1}{\pi} \left\{ (\beta - \alpha) + \frac{[\sin 2\alpha - \sin 2\beta]}{2} \right\}}$$

(ii) The fundamental component of load voltage

$$a_1 = \frac{V_m}{2\pi} [\cos 2\alpha - \cos 2\beta]$$

$$b_1 = \frac{V_m}{2\pi} [2(\beta - \alpha) + \sin 2\alpha - \sin 2\beta]$$

$$\theta_1 = \tan^{-1} \frac{a_1}{b_1}$$

(iii) The n^{th} component of load voltage

$$a_n = \frac{V_m}{\pi} \left\{ \frac{\cos(1+n)\alpha - \cos(1+n)\beta}{(1+n)} + \frac{\cos(1-n)\alpha - \cos(1-n)\beta}{(1-n)} \right\}$$

$$b_n = \frac{V_m}{\pi} \left\{ \frac{\sin(1-n)\beta - \sin(1-n)\alpha}{(1-n)} - \frac{\sin(1+n)\beta - \sin(1+n)\alpha}{(1+n)} \right\}$$

$$\theta_n = \tan^{-1} \frac{a_n}{b_n}$$

$$n=3, 5, 7, \dots$$

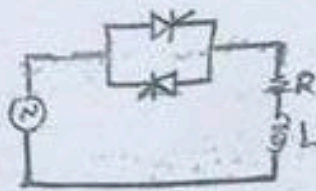
(iv) The RMS of load voltage from Fourier series

$$V_{on} = \frac{\sqrt{a_n^2 + b_n^2}}{\sqrt{2}}$$

where $n=1, 3, 5, \dots$

$$V_o = \sqrt{V_1^2 + V_3^2 + \dots + V_n^2}$$

(v) The RMS of the load current obtained from Fourier series



Single-phase Full Wave
AC Voltage Controller with
RL-Load

(1) Expressions of phase angle control

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(ii) The fundamental component of load voltage

$$a_1 = \frac{V_m}{2\pi} [\cos 2\alpha - \cos 2\beta]$$

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$$\theta_n = \tan^{-1} \frac{a_n}{b_n}$$

$n=3, 5, 7, \dots$

(iv) The RMS of load voltage from Fourier series

$$V_{on} = \frac{\sqrt{a_n^2 + b_n^2}}{\sqrt{2}}$$

where $n=1, 3, 5, \dots$

$$V_o = \sqrt{V_1^2 + V_3^2 + \dots + V_n^2}$$

(v) The RMS of the load current obtained from Fourier series

$$I_o = \sqrt{I_1^2 + I_3^2 + \dots + I_n^2}$$

Where $I_1 = \frac{V_1}{Z_1}$, $I_3 = \frac{V_3}{Z_3}$ and $I_n = \frac{V_n}{Z_n}$

$$Z_1 = \sqrt{R^2 + (\omega L)^2}, Z_3 = \sqrt{R^2 + (3\omega L)^2}, \text{ and } Z_n = \sqrt{R^2 + (n\omega L)^2},$$

$$\varphi_1 = \tan^{-1} \frac{\omega L}{R}, \varphi_3 = \tan^{-1} \frac{3\omega L}{R} \text{ and } \varphi_n = \tan^{-1} \frac{n\omega L}{R}$$

(vi) Active power

$$P = V_1 I_1 \cos(\theta_1 - \varphi_1) + V_3 I_3 \cos(\theta_3 - \varphi_3) + \dots + V_n I_n \cos(\theta_n - \varphi_n)$$

$$P = I_o^2 R$$

$$P = (I_1^2 + I_3^2 + \dots + I_n^2) R$$

(vii) Reactive power

$$Q_1 = V_1 I_1 \sin(\theta_1 - \varphi_1)$$

قوانين هذو لمتة
Fourier Series
مع ال RL-Load
1-φ AC regulator
وإذا ال R-Load only
تكون نفس القوانين
ولكن $\beta = \pi$

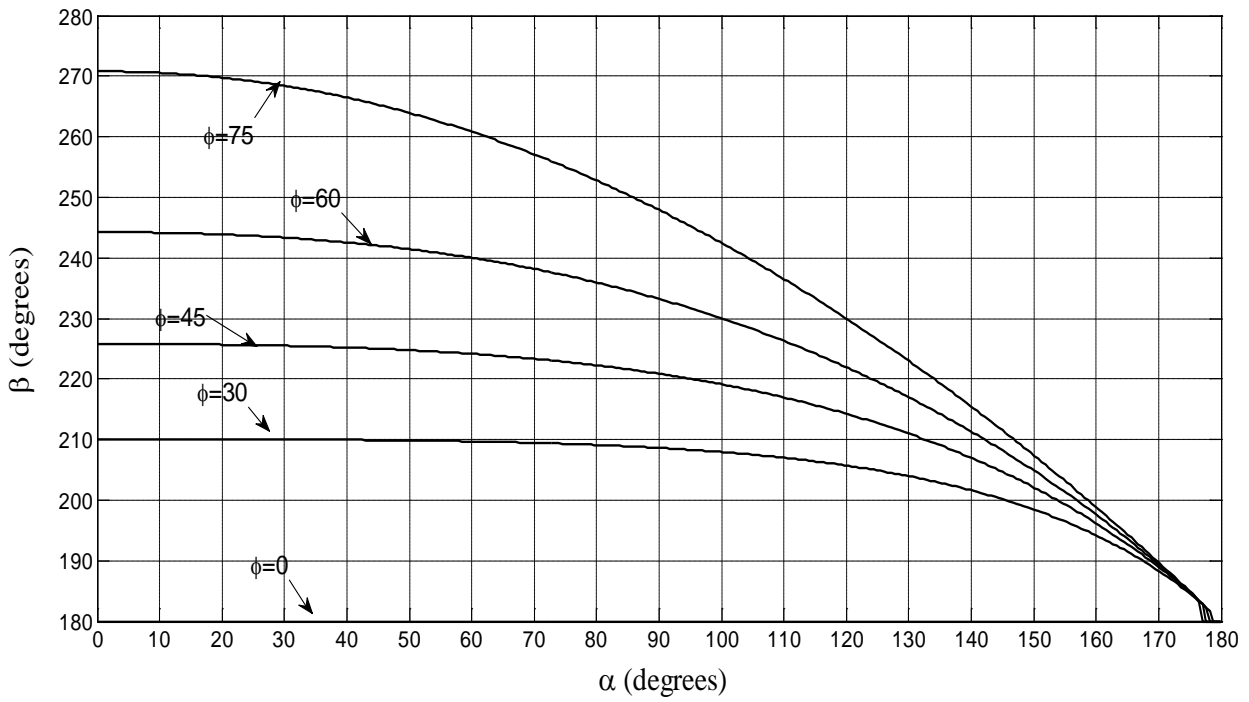


Fig. (1): Relation between *thyristor trigger delay angle* (α)
versus thyristor extinction angle (β)
(at using *RL load*)